

# Amine Structure Governs Corrosion Rates of Copper Catalysts in Electrochemical Reactive Capture of CO<sub>2</sub>

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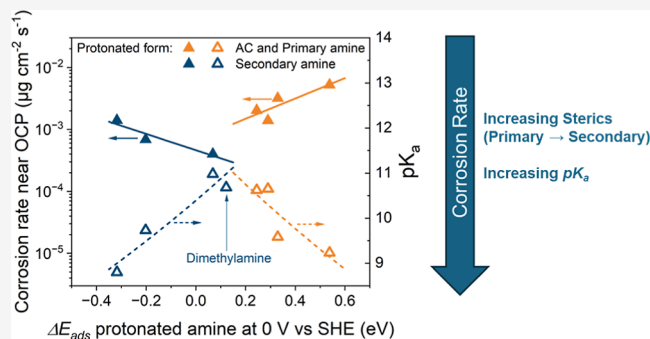


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**ABSTRACT:** Reactive capture of CO<sub>2</sub> (RCC) offers an integrated approach that combines CO<sub>2</sub> capture with its direct electrochemical conversion, eliminating the need for CO<sub>2</sub> release from the capture agent. By avoiding the pH, pressure, and temperature swings required for the release step, RCC has the potential to reduce both energy consumption and capital costs compared to the conventional sequential process of CO<sub>2</sub> capture, release, concentration, and conversion. Amines, widely used in industrial CO<sub>2</sub> capture, face challenges in RCC systems due to their incompatibility with transition metal catalysts as well as their tendency to promote electrode corrosion and parasitic hydrogen evolution. Identifying suitable combinations of amines and catalysts is therefore critical to enabling integrated CO<sub>2</sub> capture and conversion. This work systematically investigates the performance of four primary and four secondary amines for RCC on polycrystalline Cu catalysts. Among the eight tested amines, only dimethylamine showed no measurable Cu corrosion near the open circuit potential. In contrast, ammonia, methylamine, ethylamine, monoethanolamine, diethylamine, diethanolamine, and piperazine all induced Cu corrosion. Corrosion rates correlate with the pK<sub>a</sub> and steric hindrance of the amines, highlighting key parameters for catalyst–amine codesign. Grand canonical DFT calculations indicate a correlation between the adsorption strength of protonated amines, their pK<sub>a</sub>, and the extent of Cu corrosion, suggesting that both the surface binding of protonated amines and the lability of their protons play critical roles in corrosion acceleration near open circuit potentials. These findings suggest that amines with high pK<sub>a</sub> values and weak binding of their protonated forms to Cu surfaces are preferred, as they offer better corrosion resistance.



## INTRODUCTION

The rising concentration of atmospheric CO<sub>2</sub>, now exceeding 420 ppm, poses a critical threat to the environment highlighting the urgency of reaching net-zero CO<sub>2</sub> emissions by 2050 to keep global warming within safe limits.<sup>1–3</sup> Electrochemical CO<sub>2</sub> reduction (CO<sub>2</sub>R) has emerged as a promising strategy for mitigating climate change.<sup>4–6</sup> However, current CO<sub>2</sub>R systems rely on purified, pressurized CO<sub>2</sub> feedstocks, typically derived from postcombustion capture using amine-based solvents. In conventional CO<sub>2</sub> capture systems, amines cyclically absorb CO<sub>2</sub> at high-pressure and low-temperature and are regenerated at low-pressure and high-temperature. This cycle incurs high energy and capital costs due to thermal, pressure, and pH swings that destroy exergy and reduce process efficiency.<sup>7–9</sup> To enable CO<sub>2</sub> capture and utilization at global scales, more integrated and energy-efficient approaches are required.

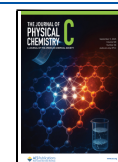
Reactive capture of CO<sub>2</sub> (RCC) offers a promising alternative by directly coupling CO<sub>2</sub> capture with electrochemical conversion, thereby eliminating the need for the energy-intensive steps of CO<sub>2</sub> separation, compression and transport.<sup>2,8–17</sup> Comparative studies between conventional CO<sub>2</sub>R systems and RCC suggest that direct amine–CO<sub>2</sub> electrolysis can deliver up to 40% energy savings by avoiding CO<sub>2</sub> thermal desorption,<sup>14</sup> with additional process integration benefits leading to a projected 12% reduction in operating costs and a 6.1% decrease in the levelized cost of CO production.<sup>15</sup> However, the successful deployment of RCC

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faces a major challenge: the incompatibility between conventional amine-based capture agents and key electrocatalysts, particularly copper (Cu), which is essential for producing multicarbon products. Understanding and overcoming this incompatibility is critical to realizing the full energy and cost benefits of RCC.

Amines remain the most utilized CO<sub>2</sub> capture agents and are increasingly explored in RCC applications.<sup>15,18–28</sup> For instance, Shen et al. demonstrated that in Ag-based RCC systems, freely dissolved CO<sub>2</sub> serves as the primary carbon source for electrochemical reduction, while amine–CO<sub>2</sub> adducts are likely to contribute as a secondary carbon source only at highly negative applied potentials.<sup>21</sup> Similarly, Leverick et al. investigated the pH-dependent speciation of CO<sub>2</sub> in monoethanolamine capture solutions and confirmed that dissolved CO<sub>2</sub> dominates electrochemical activity on Ag catalysts.<sup>22</sup> Other studies have investigated how temperature, catalyst porosity, and cation concentration affect CO production in RCC systems.<sup>23,27</sup> However, across these studies, the amine–CO<sub>2</sub> adduct is not the principal electroactive species, underscoring the need for catalyst–capture agent pairs that can directly activate these adducts for reduction. While numerous studies have underscored the potential for the use of amines in RCC systems, the electrochemical upgrading of amines has primarily focused on the use of silver catalysts.<sup>18,21–23,26</sup> Cu catalysts, however, are of paramount importance in CO<sub>2</sub> reduction research due to their unique selectivity for the selective formation of high-value C<sub>2+</sub> products, for which insights from silver catalysts do not necessarily apply.<sup>4,29,30</sup> Although the use of Cu catalysts in RCC applications has begun to be explored, hydrogen remains the predominant product under aqueous conditions, and the physicochemical principles that drive changes in the activity and stability of Cu during electrochemical RCC remain poorly understood.<sup>31–33</sup>

Recent work from our group showed that Cu and Sn corrode during the electrochemical upgrading of an ammonia carbon capture solution near the open circuit potential, while metals like Ag, Au, and Ti are immune to corrosion under the same conditions.<sup>31</sup> While Cu corrosion in the presence of amines, and other N-containing molecules has been studied in the context of electrochemical corrosion and metal protection, its implications for RCC applications are less well understood.<sup>34–40</sup> The introduction of CO<sub>2</sub> in amine-based RCC solutions further complicates the study of electrochemical corrosion as noninnocent carbamates and carbonates modify local pH values and speciation. Strmčnik et al. showed that copper dissolution in CO<sub>2</sub>-free ammonia solutions has a reaction order of 2 with respect to ammonia and proposed a two-step passivation mechanism involving Cu<sub>2</sub>O formation as the primary corrosion pathway at potentials near the onset for Cu-oxidation.<sup>35</sup> On the other hand, Kumar et al. found that amino acids inhibit copper corrosion by forming stable chemical bonds with copper surfaces through multidentate bonding via amine (–NH<sub>2</sub>) and carboxyl (–COOH) groups.<sup>40</sup> Their DFT study showed glutathione to have the highest corrosion inhibition efficiency among the amino acids tested, and this aligned with experimental trends that suggest that adsorption and passivation of surfaces is more effective for molecules with stronger electron donation through the lone pairs on the N- and O atoms in the amino acids.<sup>40</sup> Surface adsorption and chemical bond formation between amine capture agents and the Cu surface, however, may be

detrimental in RCC electrochemistry as this could interfere with the catalysis. The role of CO<sub>2</sub>-adducts in determining catalysis and stability under applied potential is not understood. Compounding the challenge, Cu surfaces are known to restructure dynamically under CO<sub>2</sub>R conditions,<sup>41–44</sup> and such restructuring may be further influenced by amine–metal interactions and CO<sub>2</sub> adduct–metal interactions.<sup>45</sup> Therefore, rational codesign of amine capture agents and Cu catalysts for RCC demands a detailed understanding of how amines, carbamates, and carbonates interact with the catalyst surface under operating conditions.

While various components of RCC systems have been studied in isolation, a fundamental challenge lies in the codesign of amine capture agents and Cu catalysts. This design space is constrained by two principal issues: (i) amine-induced corrosion of Cu surfaces, and (ii) promotion of the parasitic hydrogen evolution reaction (HER) promoted by amines and their CO<sub>2</sub> adducts. These phenomena reduce catalyst durability and suppress the formation of carbon-based products, limiting the efficacy of RCC. Despite growing interest in amine-based RCC, there is a lack of mechanistic insight into how specific molecular properties, particularly acidity (pK<sub>a</sub>) and steric hindrance, govern Cu corrosion and catalytic performance under operating conditions.

In this work, we address this gap by systematically evaluating how the molecular structure of eight commonly used amines (four primary and four secondary) affects corrosion rates and electrocatalytic behavior on polycrystalline Cu under RCC conditions. The selected amines span a range of steric and electronic properties, including ammonia and alkyl amines, as well as monoethanolamine, diethanolamine, and piperazine that represent industrial amines for CO<sub>2</sub> capture. Using electrochemical quartz crystal microbalance (eQCM) measurements, we monitor Cu mass changes as a function of potential and time. We computed binding energy descriptors to systematically model all eight amines, aiming to provide a practical framework to probe the complex environment of the RCC system and enable rapid screening of suitable sorbents for RCC. This approach has been successful in correlating theoretical calculations with experimental observations in CO<sub>2</sub>R,<sup>46–48</sup> but it still remains a challenge in RCC. Through the use of grand canonical DFT calculations we identify the binding energy of adsorption of the protonated amine as a predictive descriptor of corrosion behavior, and propose structure–function relations that can inform future codesign strategies for more effective and stable RCC systems.

## ■ METHODS

**Catalyst Preparation.** For eQCM corrosion research, Cu films were deposited via sputtering onto Au-coated quartz crystals. Oak Ridge National Laboratory supplied all the sputtered films for experimental use. The metal targets were 2 in. diameter discs (Kurt Lesker, 99.999%). During sputtering, the target-to-substrate distance was maintained at 7.5 cm. The vacuum chamber was pumped down to a base pressure of 5 × 10<sup>–7</sup> Torr for at least 3 h prior to introducing Ar gas (99.999%, AirGas). The system was then stabilized at a pressure of 20 mTorr, and plasma was ignited and sustained using a 20 W DC power source. Each sample film had a thickness of 300 nm.

In the RCE experiments, Cu cylinder electrodes (99.99% purity, 12 mm outer diameter, 8 mm length, from Pine Research Instrumentation) with a geometric area of 3 cm<sup>2</sup> were initially polished using 600 grit sandpaper, followed by a

fine polish with 0.05  $\mu\text{m}$  alumina on a microcloth pad. After sonication in distilled water, the Cu was electropolished in concentrated *o*-phosphoric acid ( $\geq 85\%$  HPLC grade, Fisher Chemical) at 1.6 V versus a Cu counter electrode for 5 min.

**Electrolyte Preparation.** Different amine concentrations were used in this work and these are indicated in the caption next to each experimental result. 4.0 M aqueous stock solutions of all the amines were first prepared for the  $\text{CO}_2$  loading experiments, except for ammonia and some of the dimethyl amine solutions where the starting amine forms were ammonium carbamate and dimethylammonium dimethylcarbamate salts. The captured solution was then diluted to 0.5 M for all the eQCM corrosion studies and to 0.2 M for the electrochemical characterization studies in our RCC cell.

The 4.0 M solutions for  $\text{CO}_2$  loading were prepared by diluting the as-received amines (methylamine ( $\text{CH}_3\text{NH}_2$  40 wt % solution in water, Sigma-Aldrich), ethylamine ( $\text{CH}_3\text{CH}_2\text{NH}_2$  70 wt % solution in water, Sigma-Aldrich), monoethanolamine ( $\text{NH}_2\text{CH}_2\text{CH}_2\text{OH}$  98%, Sigma-Aldrich), dimethylamine ( $(\text{CH}_3)_2\text{NH}$  40 wt % in water, Sigma-Aldrich), diethylamine ( $(\text{C}_2\text{H}_5)_2\text{NH}$  99.5%, Sigma-Aldrich), diethanolamine ( $(\text{CH}_2\text{CH}_2\text{OH})_2\text{NH}$  99%, Sigma-Aldrich), piperazine ( $\text{C}_4\text{H}_{10}\text{N}_2$  99%, Sigma-Aldrich), and pyridine ( $\text{C}_5\text{H}_5\text{N}$  99.8%, Sigma-Aldrich)) in water. Potassium perchlorate ( $\text{KClO}_4$  99.99%, Thermo Fisher) and potassium hydroxide ( $\text{KOH}$  99.97%, Sigma-Aldrich) were also added as the supporting electrolyte. 2 M ammonium carbamate and dimethylammonium dimethylcarbamate electrolytes (4 mol of amines per L) were prepared by dissolving ammonium carbamate ( $\text{NH}_4\text{—NH}_2\text{CO}_2$  98%, Thermo Fisher), dimethylammonium dimethylcarbamate ( $(\text{CH}_3)_2\text{NH—(CH}_3)_2\text{NCOOH}$ , Sigma-Aldrich) in a potassium perchlorate and potassium hydroxide electrolyte. Dimethylammonium dimethylcarbamate ( $(\text{CH}_3)_2\text{NH—(CH}_3)_2\text{NCOOH}$ , Thermo Fisher) was additionally used in separate contamination control studies. The concentration of  $\text{KClO}_4$  and  $\text{KOH}$  in all solutions were 0.099 and 0.001 M, respectively. The stock solution was freshly prepared before each experiment, after which  $\text{CO}_2$  loading experiments were conducted using these solutions.

**$\text{CO}_2$  Loading Experiments.** All  $\text{CO}_2$  loading experiments were conducted in a 150 mL RDE/RRDE glass cell from Pine Research, featuring a center port (24/25) and four side ports (14/20). One side port was replaced with a dual-port gas inlet (Pine Research) to allow gas sparging into the solution. The remaining ports were sealed with PTFE stoppers (Pine Research). The capture agent solution for  $\text{CO}_2$  loading was prepared as outlined in the [Electrolyte Preparation](#) section, with a liquid volume of 50 mL used in all experiments. Mass and pH were recorded every 10 min during  $\text{CO}_2$  loading until the solution reached saturation, defined as the point when no further net  $\text{CO}_2$  mass change and pH change were observed.  $\text{CO}_2$  was bubbled through the solution at a rate of 70 sccm under atmospheric pressure. It is noted that the formation of solids and precipitates was not observed in any of our  $\text{CO}_2$  loading experiments at our operating conditions of 1 atm and 293 K. Evaporative losses were accounted for by purging Ar gas at 70 sccm and measuring mass loss to consider solvent evaporation. Net  $\text{CO}_2$  loading was determined by subtracting the mass loss due to solvent evaporation (from Ar bubbling) from the mass change recorded during  $\text{CO}_2$  loading (from  $\text{CO}_2$  bubbling) as described below.

$\alpha$  = net  $\text{CO}_2$  loading (mol of  $\text{CO}_2$ /mol of amine)

$$= [(\text{mass change from } \text{CO}_2 \text{ bubbling} - \text{mass change from Ar bubbling})/44]/[\text{mol of capture agent used}]$$

All the  $\text{CO}_2$ -loaded amine solutions were purged with argon at 50 sccm for 15 min to remove as much dissolved  $\text{CO}_2$  as possible before doing electrochemistry. We note that the calculated  $\text{CO}_2$  loading does not reflect the exact  $\text{CO}_2$  loading under the operational conditions of the RCE and eQCM tests, as a dilution step of amine solution is required during experiments. The actual  $\text{CO}_2$  loading during RCE experiments can be determined through the VLE model based on the measured pH and the partial pressure of  $\text{CO}_2$  in the cell's headspace during electrochemical testing. In this work  $\text{CO}_2$ -loaded amine solutions refers to solutions after  $\text{CO}_2$  loading at 1 atm and Ar purging for 15 min. A schematic workflow is provided in the Supporting Information ([Figure S17](#)). The uniqueness of the  $\text{CO}_2$  loading method used here is not related to the  $\text{CO}_2$  capture process itself, but to being able to track mass changes and pH changes during both the  $\text{CO}_2$  capture and reduction process and identify the active species getting reduced during RCC.

**Corrosion Experiments.** All electrochemical stability tests were conducted on fresh Cu films sputtered onto Au-coated eQCM crystals. A commercially available eQCM cell from Gamry was used, employing the same setup as in previous study.<sup>31</sup> This setup with the eQCM cell enabled a systematic analysis of corrosion on Cu in various amine solutions, dependent on the applied potential. Corrosion rates were measured in two stages. First, 7 mL of a 0.099 M potassium perchlorate and 0.001 M potassium hydroxide solution was added to the eQCM cell. Once a stable potential was achieved with this supporting electrolyte at the designated current, 1 mL of amine stock solution (prepared as outlined in the [Electrolyte Preparation](#) section) was introduced to reach a final amine concentration of 0.5 M. Corrosion rates were measured after the amine solution was added to the eQCM cell. Each corrosion rate experiment was repeated at least once.

**Electrochemical Characterization.** The RCC experiments were carried out using an RCE cell which is a device previously used by our group to determine the contributions from dissolved  $\text{CO}_2$  and  $\text{CO}_2$ -capture agent adduct for RCC on transition metals. A 76 mL volume of supporting electrolyte was introduced into the RCE cell, and a constant current of  $-4 \mu\text{A cm}^{-2}$  was applied under a constant flow of Ar at 20 sccm. Next, 4 mL of the amine stock solution was then added to prevent the Cu electrode from being exposed to amine species at open circuit potential. Once the potential and  $\text{CO}_2$  partial pressure stabilized following the addition of the amine, chronopotentiometry was conducted at a constant current of  $-12 \text{ mA cm}^{-2}$  with continuous Ar flow. In each experiment, five gas GC injections were obtained, with the average of the final four injections used for analysis and representation in all figures. Additionally, the partial pressure of  $\text{CO}_2$  in the cell headspace was measured with each GC injection to determine the equilibrium concentration of dissolved  $\text{CO}_2$  with the captured  $\text{CO}_2$  in the bulk electrolyte. Diluting the stock solution to 0.2 M for the RCE experiments allows us to measure the  $\text{CO}_2$  peak in the GC and consequently quantify the amount of dissolved  $\text{CO}_2$  present in the system, the  $\text{CO}_2$  loading, and the speciation using VLE models. Higher concentration amine solutions hold more  $\text{CO}_2$  into it, resulting

in the overloading of the GC FID detector hindering the CO<sub>2</sub> peak quantification. We have tracked the pH after dilution to confirm that the CO<sub>2</sub> loading does not change in this process (Figure S7). Electrochemical impedance spectroscopy (EIS) was performed, and the uncompensated resistance was determined from the real component of the resistance measured at high frequencies ( $f \geq 100$  kHz). This resistance was subsequently used to correct all chronopotentiometry data.

**Product Characterization.** An online GC is used to detect and quantify gaseous products during the experiment. Injections from the cell headspace were taken every 20 min. A sampling cycle includes a 14 min phase for separation and quantification of products followed by a 6 min cooling interval. Details on the procedure for product quantification are given in our previous report.<sup>31</sup>

**NMR Analysis.** All NMR spectra were collected with Bruker NEO 600 spectrometer. NMR samples were prepared by mixing 700  $\mu$ L of the sample with 105  $\mu$ L of a D<sub>2</sub>O/TMSP-*d*<sub>4</sub> solution as an internal standard. The internal standard solution was prepared by mixing 1 mL of deuterium oxide (D<sub>2</sub>O, 99.9%, EMD Millipore) with 15 mg of 3-(trimethylsilyl)propionic-2,2,3,3-*d*<sub>4</sub> acid, sodium salt (TMSP-*d*<sub>4</sub>, 98+ atom % D, Sigma-Aldrich).

**Physical Characterization.** Scanning electron microscopy (ZEISS Supra 40VP SEM) was used to analyze the morphology and microstructures of the sputtered Cu films before and after corrosion experiments with ammonium carbamate.

**Slab Model.** The Cu(111) surface was modeled with a cell dimension of about 15  $\text{Å} \times 15 \text{Å}$ . The bottom two layers were constrained as the rigid interior, and everything else was allowed to relax as the catalytic interface. A vacuum layer of 40  $\text{Å}$  was added under the periodic boundary condition.

**DFT Methods.** DFT calculations were performed using the VASP program (version 5.4.4), with the RPBE functional,<sup>49</sup> DFT-D3 dispersion correction,<sup>50</sup> and PBE\_PAW pseudopotentials.<sup>51</sup> The cutoff energy for the plane-wave basis set was set to 400 eV, and Gaussian smearing with a width of 0.1 eV was used. The convergence criterion for electronic minimization and geometry optimization were set to 10<sup>-6</sup> eV and 0.02 eV/ $\text{Å}$ , respectively. Only the gamma *k*-point sampling in the reciprocal space of the Brillouin zone was used due to the large supercell used.

**Grand Canonical DFT (GCDFT).** To calculate the adsorption energy as a function of electrochemical potential, the catalytic interface of the electrode was treated as a grand canonical ensemble of electrons. Different amounts of electrons are used to shift the work function and sample the free energy surface. The surface charging technique<sup>52</sup> was used to calculate the potential-dependent, grand canonical free energy of the surface,  $\Delta G$ , which is given by

$$\Delta G(U^{\text{VAC}}) = \Delta E^{\text{elec}}(U^{\text{VAC}}) - q(U^{\text{VAC}})FU^{\text{VAC}}$$

where  $\Delta E^{\text{elec}}(U^{\text{VAC}})$  is the electronic energy at potential  $U^{\text{VAC}}$ , the vacuum scale potential of the electrode,  $q$  is the number of supplied electrons to the system, and  $F$  is the Faraday constant. The system's work function was computed relative to the initial charge of the adsorbate. By treating the catalytic interface as an ideal capacitor,  $\Delta G$  can be approximated by

$$\Delta G(U^{\text{VAC}}) \approx \Delta E^{\text{elec}}(U_0^{\text{VAC}}) - \frac{1}{2}C(U^{\text{VAC}} - U_0^{\text{VAC}})^2$$

where  $U_0^{\text{VAC}}$  is the vacuum scale zero charge potential, and  $C$  is the effective capacitance.  $U^{\text{VAC}}$  can be converted to the potential with respect to the standard hydrogen electrode,  $U^{\text{SHE}}$  by

$$U^{\text{SHE}} = U^{\text{VAC}} - 4.44$$

VASPsol,<sup>53</sup> a linearized Poisson–Boltzmann implicit solvation model, was used to represent the polarizable electrolyte region. The dielectric constant of water was used and set to 78.4. The Debye screening length was set to 3  $\text{Å}$ , which corresponds to 1 M concentration of electrolytes evaluated by

$$\lambda \approx \frac{3}{\sqrt{I}} \text{Å}$$

where  $I$  is the ionic strength in M.<sup>52</sup> The slabs were symmetrized to avoid asymmetric potential in the polarized solvation region, and the thickness of the solvent was set to 90  $\text{Å}$ .

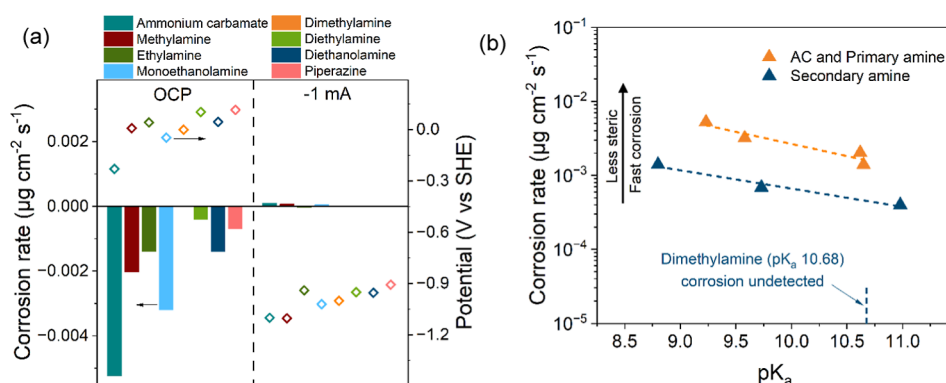
**Adsorption Energies Calculations.** The adsorption geometry was first sampled and optimized at different binding sites. The GCDFT free energy of adsorption of the most stable configurations were calculated by

$$\Delta G_{\text{ad}}(U^{\text{SHE}}) = \Delta G(U^{\text{SHE}}; *_{\text{ad}}) - \Delta G(U^{\text{SHE}}; *) - E(\text{ad})$$

where  $*$  denotes the electrode–electrolyte interface and  $\text{ad}$  denotes the adsorbate.

## RESULTS AND DISCUSSION

To investigate the interaction between Cu catalysts and CO<sub>2</sub>-loaded amines at the electrode surface, we measured Cu corrosion rates in the presence of eight amine-based capture agents using an electrochemical quartz crystal microbalance (eQCM). The tested solutions included CO<sub>2</sub>-loaded ammonia, methylamine, ethylamine, monoethanolamine, dimethylamine, diethylamine, diethanolamine, and piperazine. The ammonia carbon capture solution was prepared by dissolving ammonium carbamate (AC) in water, while all other amine capture solutions were prepared by loading CO<sub>2</sub> into the free amine forms prior to the eQCM experiments. CO<sub>2</sub> loading experiments were performed by flowing 70 sccm of CO<sub>2</sub> into each amine solution. During CO<sub>2</sub> loading, the mass and pH changes were tracked until CO<sub>2</sub> saturation was reached (Figures S1 and S2). The amine solutions take around 100 min to be fully loaded with CO<sub>2</sub> and to reach equilibrium with a partial pressure of CO<sub>2</sub> of 1 atm (Figure S1). Larger mass changes correspond to higher CO<sub>2</sub> loadings. The pH of the solutions quickly decreases from highly alkaline values (pH of 11.5–13.5, depending on the amine) during the first few minutes of CO<sub>2</sub> loading (Figure S2) and eventually reaches an equilibrium pH value of between 7 and 9 after 100 min. The final pH value is that of the amine solution in equilibrium with a partial pressure of CO<sub>2</sub> of 1 atm at room temperature.<sup>27</sup> Figure S3 shows the net CO<sub>2</sub> loading value ( $\alpha$ ) of amines after the CO<sub>2</sub> loading experiment. Here,  $\alpha$  corresponds to the mol of captured CO<sub>2</sub> per mol of amine. CO<sub>2</sub> loading values range between 0.5 and 0.9 for the different amines and correspond to the maximum loading values achievable under a CO<sub>2</sub> partial pressure of 1 atm at room temperature. After loading, all solutions were purged with Ar at 50 sccm for 15 min to remove as much dissolved CO<sub>2</sub> as possible before doing electrochemistry. This does not mean that all the dissolved CO<sub>2</sub> is removed, as the solution rapidly equilibrates to release CO<sub>2</sub>



**Figure 1.** (a) The corrosion rates (bars) and measured potentials (dots) of sputtered Cu films after the exposure to CO<sub>2</sub>-loaded 0.5 M amine solutions near the open circuit potential and under a current density of  $-1 \text{ mA cm}^{-2}$ . (b) The corrosion rate values versus the  $\text{pK}_a$  for investigated amines. The corrosion rate of dimethylamine, showing no detectable corrosion behavior, is not plotted.

when the partial pressure of CO<sub>2</sub> in the headspace is decreased. We have previously shown that the quantification of CO<sub>2</sub> in the headspace of the electrochemical cells under Ar flow and the pH of the solution can be used to estimate the concentration of dissolved CO<sub>2</sub> in solution during electrochemistry.<sup>27</sup> In addition to determining the concentration of dissolved CO<sub>2</sub>, the use of vapor–liquid equilibrium (VLE) models can also be used to determine speciation. Figure S4 shows the change in mass and pH as a function of time for an experiment where Ar was purged for 90 min after CO<sub>2</sub> loading in a 4 M MEA solution. The pH and CO<sub>2</sub> loading reach a new quasi-steady state as the capture solution starts to stabilize with the low partial pressure of CO<sub>2</sub> under the Ar flow in the cell overhead. While the pH increases and the loading decreases, the VLE model tracks the change in speciation and allow us to start to close the gap in relating activity and performance to speciation in the RCC electrolyte under dynamic operation.

During the eQCM experiments, we have measured the initial mass change rates for polycrystalline Cu thin films in the presence of each amine at a constant current of  $-1 \mu\text{A cm}^{-2}$  (near open circuit potential, OCP) and  $-1 \text{ mA cm}^{-2}$  (representing electrocatalytic reduction conditions). The potential and mass change rates during these experiments are shown in Figure 1a. In our previous work,<sup>31</sup> we observed that the addition of ammonium carbamate to a solution of potassium perchlorate electrolyte led to the corrosion of the Cu film near OCP, and we also observed the formation of a coordination complex between Cu ions and ammonia molecules in the bulk of the solution. Optical and SEM images of the sputtered Cu films before and after corrosion with ammonium carbamate are shown in Figure S22. Similarly, Cu exhibited corrosion behavior from all the tested amines, except for dimethylamine. Corrosion rates range from approximately  $-0.0004$  to  $-0.005 \mu\text{g cm}^{-2} \text{ s}^{-1}$  for the sputtered Cu thin films near OCP. The time-dependent changes in mass and applied potential for each amine under the two selected constant current conditions are shown in Figures S5 and S6. At the low currents, near the open circuit potential, the potential measured ranges from 0.15 to  $-0.3 \text{ V vs SHE}$ . At the most cathodic currents of  $-1 \text{ mA cm}^{-2}$ , the potential measured ranges from  $-0.9$  to  $-1.2 \text{ V vs SHE}$ . While Cu corrosion is generally observed at conditions near OCP, a slight increase in the mass was observed for all the amines under the more cathodic potential and could be indicative of the adsorption of species in solution and strong interactions between the Cu surface and the amine capture agents. At the

most negative potentials and under high current densities and local pH values, amines could compete with electrolyte cations for space in the double layer, particularly if there are favorable adsorption interactions that could drive amines to bind and linger for longer at the catalyst surface.

From the experimental observations summarized in Figure 1a, we can identify three principal (though to some extent interdependent) characteristics of amine capture agents that impact Cu corrosion behavior. These are (i) steric effects, (ii) the acidity of the amine's conjugate acid, and (iii) the nucleophilicity of nitrogen within the amine structure. The observed corrosion behavior arises from the combined action of these effects.

First, less steric hindrance in amines leads to accelerated Cu corrosion. As illustrated in Figure 1b, the corrosion rates of secondary amines (blue triangles) are lower than those of ammonia and primary amines (orange triangles). This indicates that sterically hindered amines physically limit access to the electrode surface and impede electron donation which can eventually slow down the corrosion reaction of the Cu catalyst near the open circuit potential.<sup>54,55</sup>

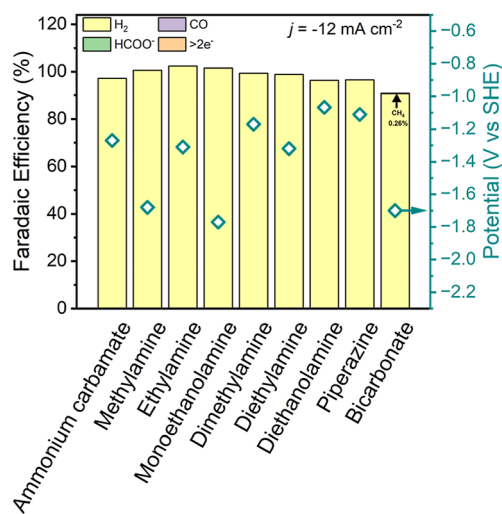
Second, corrosion rates seem to increase as the  $\text{pK}_a$  of the amine decreases. Prior to the addition of the amines to the supporting electrolyte solution (consisting of 0.099 M KClO<sub>4</sub> + 0.001 M KOH) in the eQCM cell, a constant current of  $-1 \mu\text{A cm}^{-2}$  was applied to the Cu film to bring the Cu surface to as close as possible to its metallic state. However, due to the aqueous electrolyte, the potential measured at these low cathodic currents near the open circuit potential correspond to those where Cu is thermodynamically expected to exist as Cu<sub>2</sub>O. This is based on the Pourbaix diagram of Cu in water at 25 °C, where for an aqueous solution with a pH of 10.2 the thermodynamically stable form at potentials between 0.0 and 0.2 V vs SHE is Cu<sub>2</sub>O.<sup>56</sup> Upon the addition of the amine solution, the measured pH in the eQCM cell drops and is lower than the respective  $\text{pK}_a$  values of the amines (Figure S7), and thus a high concentration of protonated amines is expected in the solution. The  $\text{pK}_a$  values of the amines used in the stability tests and the pH of the corresponding amine solutions are shown in Figure S7. Upon the introduction of the amine solution under these conditions, protonated amines can react with the surface oxide layer near the open circuit potential, facilitating the generation of Cu<sup>2+</sup> ions.<sup>34</sup> Free amines coordinate with Cu<sup>2+</sup> ions due to their high Lewis basicity, leading to the solvation of the Cu–amine complex.<sup>35</sup> Therefore, amines with lower  $\text{pK}_a$  values, and thus stronger

conjugate acids, are more efficient at driving acid–base reactions with the oxide surface, resulting in accelerated Cu corrosion. This leads to more positive potentials being required to sustain a constant current density in the eQCM experiments upon the addition of the CO<sub>2</sub>-loaded amine solutions (Figures S5 and S6).

Lastly, strong nucleophilicity of nitrogen in the amine structure increases the reactivity of the amines for corrosion. For example, we observe that dimethylamine, with a slightly lower pK<sub>a</sub> and less sterically hindered nitrogen atom than diethylamine, did not induce Cu corrosion in our eQCM experiments. This, we hypothesize, is due to the fact that the larger alkyl group of diethylamine imparts a greater electron-donating inductive effect on the nitrogen atom, thus increasing the nucleophilic attack of the diethylamine on the Cu atoms compared to the dimethylamine. Steric factors play a considerably greater role in the nucleophilicity for secondary amines than for primary amines.<sup>57</sup> The stronger electron-donating substituents stabilize the initial adsorption of amines on the Cu surface by increasing their reactivity to the amine, thereby facilitating the formation of Cu–amine complexes.<sup>45</sup>

At the more cathodic potentials, eQCM measurements did not reveal any corrosion behavior on Cu films under all tested amine solutions. In the potential range between  $-0.9$  V and  $-1.4$  V vs SHE, Cu remains in its metallic state, rendering it highly immune to corrosion.<sup>56</sup> This explains why, following the initial mass step jump upon amine addition, the mass change rate of Cu remains near zero under reductive conditions. However, the absence of corrosion in our eQCM results does not necessarily imply that Cu is completely unreactive with the amines. Recently, Guan et al. demonstrated that amine ligands in solution can directly chemisorb onto the Cu electrode, coordinate with the metal center, and induce the rearrangement of the Cu surface by extracting Cu as adatoms in low coordination sites. These amine ligands can further stabilize surface copper–ligand complexes even under negative potential conditions.<sup>45</sup> Therefore, the initial mass increase immediately after amine addition could potentially be explained by the binding of amine ligands on the Cu surface. This interaction can alter the electronic structure of the catalyst, influencing how the Cu catalyst reacts with intermediates, shifts reaction pathways, or even partially blocks active sites on the Cu surface due to amine ligands. Having established the corrosion behavior of Cu in CO<sub>2</sub>-loaded amine solutions, we next investigated whether these surface interactions also influence the electrocatalytic performance of Cu for CO<sub>2</sub> reduction under RCC conditions.

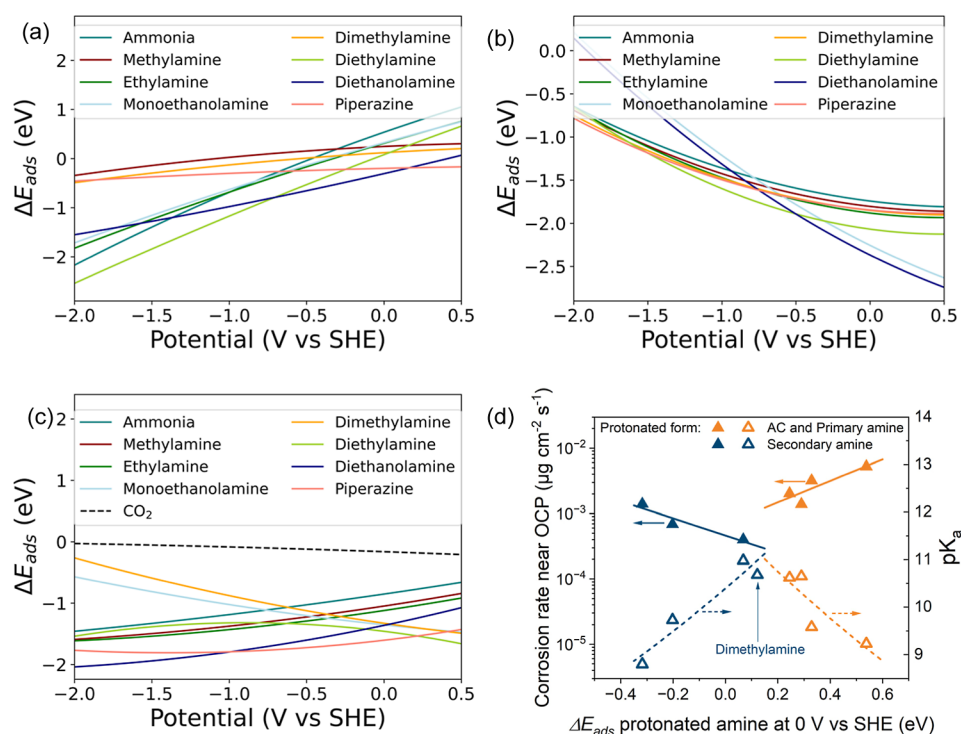
The same amines tested with the eQCM for stability studies were investigated for the electrochemical reduction of captured CO<sub>2</sub> at a constant current density of  $-12$  mA cm<sup>-2</sup> under constant Ar flow. The electrochemical reduction of potassium bicarbonate electrolyte under Ar flow was used as a reference. Figure 2 shows the Faradaic efficiencies observed for the different capture agents on Cu electrodes. The sum of the Faradaic efficiencies is higher than 95% and the only observed product is hydrogen for all cases when using 0.2 M of the CO<sub>2</sub>-loaded amine solvents, while 0.21% of CH<sub>4</sub> was detected from 0.2 M bicarbonate electrolyte. Detailed descriptions of products and Faradaic efficiencies are shown in Table S1 in the Supporting Information. In our observation, the applied potentials are a function of HER kinetics which is a more facile reaction than CO<sub>2</sub>R or RCC. Some amines have a higher propensity to form H<sub>2</sub> than others, and this depends on the



**Figure 2.** Faradaic efficiency for direct electrochemical reduction of 0.2 M amine solution electrolytes under Ar flow at 20 sccm. The right y-axis shows surface potential vs SHE. RCE experimental conditions: The rotation rate of the cylinder electrode in the RCE cell is 800 rpm, the constant current is  $-12$  mA cm<sup>-2</sup>, and the electrochemical cell temperature is 20 °C.

intrinsic pK<sub>a</sub> of the amine (i.e., the dissociation kinetics of the amines in aqueous solutions), and the sterics of the amine (i.e., how hindered the molecule is to undergo reduction near the surface of the electrode). It is hard to determine which factor plays a bigger role in HER as there are other species, like bicarbonate and water, that are present simultaneously in the solution and also contribute to HER. Furthermore, the speciation as discussed in this paper is a function of CO<sub>2</sub> loading, pH, temperature, and pressure. Therefore, more detailed study by varying the pH, partial pressure and amine concentrations is needed to elucidate the exact mechanism of HER in RCC systems.

As established in our previous research, the carbon products generated under RCC conditions arise from the electrochemical reduction of dissolved CO<sub>2</sub> rather than from the reduction of amine–CO<sub>2</sub> adducts, so the amount of carbon product is proportional to the partial pressure of CO<sub>2</sub>.<sup>21</sup> It is noted that while Cu can produce CH<sub>4</sub> from bicarbonate, it does not generate carbon-based products in amine solutions even when the CO<sub>2</sub> partial pressures and consequently the amounts of dissolved CO<sub>2</sub> are comparable or higher than those in the bicarbonate solution (Figure S8). Although the reduction of dissolved CO<sub>2</sub> is thermodynamically favorable under RCC operating conditions, the complete absence of carbon products on Cu is noteworthy despite the high loading of CO<sub>2</sub> in the system (0.5 to 0.9 mol of CO<sub>2</sub> per mol of amine). GC data from a blank injection taken before the start of electrolysis (when the  $j = -4$  μA cm<sup>-2</sup>, near OCP), and an injection during RCC electrolysis at  $j = -12$  mA cm<sup>-2</sup> are shown in Figures S9 and S10 for each of the amines in Figure 2. For comparison, the GC data for bicarbonate is shown in Figure S11 where methane is observed as the minor product, while the GC peak is well above the detection limit. The complete absence of any carbon product on the Cu catalyst may result from strong interactions between the amine ligands and the Cu surface, which could deactivate or block active sites responsible for CO<sub>2</sub> reduction on the Cu catalyst. Further



**Figure 3.** Adsorption energies,  $\Delta E_{\text{ads}}$ , of (a) the protonated form, (b) the  $\text{CO}_2$  adduct, and (c) the neutral form, as well as  $\text{CO}_2$ , of the investigated amines on Cu as a function of electrochemical potential. (d) Experimental corrosion rate near OCP (left axis), and  $\text{pK}_a$  values (right axis) of primary and secondary amines as a function of the calculated adsorption energy of the protonated form at 0 V vs SHE.

investigation is required to fully elucidate this interaction and its impact on RCC systems.

Recently, methane has been reported as a product of carbamate reduction on Au supported catalysts.<sup>28</sup>  $\text{CH}_4$  production on bare gold was attributed to single atom impurity sites, while CO selectivity was preferred when metal impurities were removed using a chelating agent, indicating that  $\text{CH}_4$  formation can be driven by the presence of impurities while not being the result of direct carbamate electroreduction.

Initial experiments on the reduction of 0.2 M dimethylammonium dimethylcarbamate solution using Cu electrodes in our RCE cell also showed traces of methane with Faradaic efficiencies (F.E.) for  $\text{CH}_4$  of about 0.035%. Although these amounts only correspond to 1–2 ppm of  $\text{CH}_4$  in the headspace of the cell, the mechanistic implications of  $\text{CH}_4$  formation coinciding with the lack of corrosion of the Cu surface were interesting, as these both were unique to dimethylamine. Further investigation, however, revealed that the partial current densities of  $\text{CH}_4$  were independent from the applied potentials (Figure S12) and that any catalytic activity for  $\text{CO}_2$  reduction could be eventually attributed to metal impurities in the carbamate reagent. Using ICP–MS measurements on the electrolyte solution we observed that commercially available dimethylcarbamate solutions contained high levels of Fe, Ca, and Pt impurities which could be the potential reasons for the trace amounts of  $\text{CH}_4$  that is produced (Table S2). To verify this, we used dimethylamine solution and loaded it with  $\text{CO}_2$  by bubbling it into the solution at 1 atm (Figure S13). We conducted the same electrochemical experiments on this prepared solution and did not see any  $\text{CH}_4$  production as shown in Figure S13, despite having nominally the same major speciation in the solution as that of the 0.2 M dimethylammonium dimethylcarbamate electrolyte (Figure S14). The only product observed was  $\text{H}_2$ .

To further investigate the role of the impurities identified in Table S2 (Fe, Ca, and Pt), we intentionally introduced Fe and Ca into the  $\text{CO}_2$ -loaded dimethylamine solution to assess their impact on  $\text{CH}_4$  production (Figure S15). However, we were unable to detect any  $\text{CH}_4$ , and experiments with the intentional addition of Pt were not pursued as these could cause a contamination of our experimental setup. Rather than trying to identify if Pt was the source of the low activity for  $\text{CH}_4$ , we performed electrochemical reduction experiments using dimethylcarbamate from an alternative supplier under the same conditions as the experiment where  $\text{CH}_4$  was initially observed, yet, no  $\text{CH}_4$  production was detected (Figure S16). This suggests that the  $\text{CH}_4$  observed was due to the presence of impurities in the as-purchased carbamate salt and not the reduction of the carbamate on Cu. These findings reinforce that trace methane formation is not an intrinsic feature of dimethylamine-based RCC chemistry, and highlight the importance of using high-purity reagents when evaluating  $\text{CO}_2$  electroreduction performance in RCC systems. More detailed discussion on the role of impurities in RCC is presented in the Supporting Information.

To gain theoretical insights into the experimentally observed corrosion behavior, we performed grand canonical DFT (GCDFT) calculations to determine the potential-dependent adsorption energies of three species: the protonated form, the  $\text{CO}_2$  adduct, and the neutral form of each amine. As shown in our previous work,<sup>31</sup> common descriptors used in  $\text{CO}_2\text{R}$  are inadequate in rationalizing the activity and stability in RCC. Therefore, we have calculated the binding energy specifically related to the speciation of the amine to rationalize the corrosion behavior observed in the experiments. The system's work function was computed relative to the initial charge of the adsorbate, as described in the Methods section, and the optimized geometries are provided in Figures S18–S20.

Since the adsorption energy represents the thermodynamics of the binding of an isolated adsorbate when it is present at the interface, the bulk speciation at different applied potentials should also be considered to determine the availability of species at the interface. Given that the equilibrium pH (Figure S2) is lower than the  $pK_a$  of all studied amines (Figure 1b), a substantial fraction of each amine is protonated under RCC conditions. These protonated species dominate near the open circuit potential, while under more negative, cathodic potentials, the dominant amine species at the catalyst–electrolyte interface may shift to either the neutral amine or the  $\text{CO}_2$  adduct,<sup>26</sup> depending on buffering kinetics and transport rates under the local high pH conditions. Thus, protonated amines are key to understanding corrosion near OCP, whereas the neutral and  $\text{CO}_2$ -adduct forms are more relevant for catalysis and electrode restructuring.

At more negative potentials relevant to electrocatalysis, all protonated amines show favorable adsorption on Cu. However, under these cathodic conditions and under the flow of current, local pH increases at the Cu surface, shifting the dominant amine species toward either the neutral form or the  $\text{CO}_2$  adduct, depending on the relative rates of transport of species in and out of the double-layer as well as the rate of the electrolyte and the amine buffering reaction kinetics. At a first approximation, the protonated form of the amine is the most relevant species for understanding corrosion near OCP, while the neutral amine and  $\text{CO}_2$  adduct are more relevant for interpreting catalysis and restructuring of electrodes under applied negative potentials.

Figure 3d reveals a correlation between the adsorption energy of the protonated amines, their  $pK_a$ , and the experimentally measured corrosion rates. Corrosion resistance is maximized when amines combine high  $pK_a$  values (weaker acidity) with moderate adsorption strengths. This balance allows surface protection without enhancing proton-mediated oxide dissolution. Amines with lower  $pK_a$  values, in contrast, more readily donate protons that facilitate oxide dissolution and promote Cu dissolution, even if their adsorption is weak. An extended discussion on why dimethylamine showed no measurable Cu corrosion near the open circuit potential is given in the Supporting Information. At the electrocatalytic potential under a current density of  $-1 \text{ mA cm}^{-2}$ , the Cu electrode becomes negatively charged, allowing favorable adsorption of cationic species. Under these conditions, protonated amines can help inhibit corrosion either by forming surface-passivating films (as evidenced by the mass increase observed in the eQCM study), or by stabilizing surface reconstructions that kinetically suppress dissolution. This is consistent with broader literature on corrosion inhibitors, where protonated amines are known to form hydrophobic protective layers that suppress metal dissolution.<sup>58–61</sup> We note that the protonated form of the amine can play an important role in its transport to the surface due to electrostatics, but that once inside of the double layer it could be deprotonated to facilitate HER leaving behind on the surface the neutral form of the amine that has an even more favorable adsorption energy on Cu (Figure 3c).

Again, while protonated amines may inhibit corrosion, they also act as proton donors that enhance the competing hydrogen evolution reaction (HER), as shown in Figure 2. In contrast, the desired reduction species in amine-based RCC, which is the  $\text{CO}_2$  adduct, experience increasing electrostatic repulsion at more negative potentials, which reduces their

surface accessibility. Consistent with this, Figure 3b shows that the adsorption strength of the  $\text{CO}_2$  adducts decreases with increasing negative potential for the investigated amines. Interestingly, monoethanolamine and diethanolamine exhibit strong adsorption near OCP but lose binding strength more rapidly under reducing conditions. This is attributed to the reduced polarizability of the hydroxyl-containing adducts, which limits their stabilization under strongly cathodic bias (Figure S19). These results suggest that rational capture agent design for RCC should consider substituent effects that modulate the adsorption of both protonated amines and  $\text{CO}_2$  adducts.

Finally, as shown in Figure 3c, neutral amines bind more strongly to Cu than  $\text{CO}_2$  itself. This likely contributes to the lack of carbon products observed experimentally, as amine coverage competes with  $\text{CO}_2$  for active sites. Taken together, these findings suggest that amine-based RCC systems face a dual challenge: protonated amines promote HER while blocking corrosion, and free  $\text{CO}_2$  and  $\text{CO}_2$ -amine adducts struggle to compete for adsorption with amines, resulting in the suppression of productive  $\text{CO}_2$  reduction. This dual inhibition mechanism provides a molecular rationale for the experimentally observed selectivity toward hydrogen and the absence of carbon-based products in Figure 2. Altogether, these insights demonstrate that the molecular factors that stabilize Cu surfaces against corrosion at negative potentials simultaneously hinder  $\text{CO}_2$  activation, underscoring a fundamental constraint in the design of amine-based RCC systems.

## CONCLUSIONS

In summary, this study systematically evaluated amine-based capture agents for their potential application in RCC systems using polycrystalline Cu catalysts. Eight primary and secondary amines were assessed for their chemical compatibility with Cu through eQCM analysis and electrocatalytic activity of Cu in these amine solutions was determined using an RCE cell with well-defined transport characteristics. Among the tested amines, only dimethylamine demonstrated compatibility with Cu, showing no corrosion near OCP, whereas all other amines led to catalyst corrosion. The  $pK_a$  and steric effects of the amines were found to directly correlate with the corrosion rates of sputtered Cu films. At more cathodic potentials, eQCM revealed no corrosion behavior due to the strong immunity of metallic Cu to corrosion with amines. However, an initial mass increase was observed immediately after amine addition, which is potentially attributed to the binding of amine ligands on the Cu surface that could affect catalysis. To mitigate corrosion in amine-based RCC, the effective adsorption of protonated amines appears crucial, as evidenced by grand canonical DFT calculations that reveal a link between their adsorption strength and the observed corrosion rates. We note that our binding energy descriptor is a simplified model of the complex double layer structure in RCC, and such calculation alone does not determine the dominant species at the interface. Future work should focus on promising sorbent candidates and employ more comprehensive models, such as *ab initio* molecular dynamics simulation with explicit solvation,<sup>62</sup> that in turn are coupled to continuum reaction-transport models to realistically model the complex local environment in RCC.

In all amine-based capture solutions, parasitic HER dominated the catalysis, with no carbon products observed,

whereas CH<sub>4</sub> production was detected in bicarbonate solutions. The absence of carbon products in amine solutions is likely due to the deactivation of Cu catalyst active sites caused by the strong interactions between amine ligands and the Cu surface. These results highlight the challenges limiting the applicability of amine-based capture agents in RCC systems and emphasize the need for further systematic investigation into novel capture agents to advance RCC systems. As a first step, we find that amines with high pK<sub>a</sub> values and weak adsorption of their protonated forms should be favored in the design of Cu-based RCC systems. Our results offer mechanistic design rules for amine–catalyst codesign in RCC and identify critical trade-offs between corrosion inhibition and catalytic accessibility. Future efforts should explore alternative families of capture agents that maintain compatibility with active catalyst sites while minimizing parasitic reactions, while also retaining practically useful kinetics for CO<sub>2</sub> capture.

## ■ ASSOCIATED CONTENT

### SI Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acs.jpcc.5c03178>.

Additional experimental details, methods, and a schematic of the experimental setup; the computational section includes all methods, structures, and computational parameters (PDF)

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## Notes

The authors declare no competing financial interest.

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